

**Research Article**

## **MHD CONVECTIVE HEAT TRANSFER OF A NANO FLUID FLOW PAST AN INCLINED PERMEABLE PLATE WITH HEAT SOURCE AND RADIATION**

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### **ABSTRACT**

We investigated theoretically the MHD flow of a nano-fluid past an inclined, oscillatory and permeable semi-infinite flat plate. The constant heat source and the thermal radiation are also considered. The slip velocity is oscillatory on time. The governing equations of the boundary layer are solved numerically using the method of lines. The influence of various parameters on velocity and heat transfer is analyzed. The increase in inclination of the plate, thinning the momentum boundary and enhancing the thermal boundary layers.

**Key Words:** Nano - Fluid, Mhd, Inclined Plate, Radiation, Method of Lines.

### **List of symbols**

$B_0$	Constant applied magnetic field ( $\text{Wb m}^{-2}$ )
$C_p$	Specific heat at constant pressure ( $\text{J kg}^{-1} \text{K}^{-1}$ )
$g$	Gravity acceleration ( $\text{m s}^{-2}$ )
$J$	Current density
$M$	Dimensionless magnetic field parameter
$n$	Dimensionless frequency
$Nu$	Local Nusselt number
$Pr$	Prandtl number
$Q$	Dimensional heat source ( $\text{kJ s}^{-1}$ )
$Q_H$	Dimensionless heat source parameter ( $\text{kJ s}^{-1}$ )
$S$	Dimensionless suction parameter
$t$	Dimensionless time (s)
$T$	Local temperature of the nano-fluid (K)
$T_w$	Wall temperature (K)
$T_\infty$	Temperature of the ambient nano-fluid (K)
$u, w$	Dimensionless velocity components ( $\text{m s}^{-1}$ )
$U_0$	Characteristic velocity ( $\text{m s}^{-1}$ )
$w_0$	Mass flux velocity
$k$	Thermal conductivity
$R_a$	Radiation parameter

### **Greek symbols**

$\alpha$	Thermal diffusivity ( $\text{m}^2 \text{s}^{-1}$ )
$\beta$	Thermal expansion coefficient ( $\text{K}^{-1}$ )
$\varepsilon$	Dimensionless small quantity ( $\ll 1$ )
$\phi$	Solid volume fraction of the nano-particles
$\mu$	Dynamic viscosity (Pa s)
$\nu$	Kinematic viscosity ( $\text{m}^2 \text{s}^{-1}$ )

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$\theta$	Dimensionless temperature
$\sigma$	Electrical conductivity ( $\text{m}^2 \text{s}^{-1}$ )
$\sigma_1$	Stefan-Boltzmann constant
$\delta$	Mean absorption Coefficient
$\gamma$	Inclination angle of the plate
$\rho$	Density

### **Superscript**

– Dimensional quantities

### **Subscripts**

f	Fluid
s	Solid
nf	Nano-fluid

## **INTRODUCTION**

Research in the field of Heat transfer challenging the cooling of many systems used in day to day life of mankind. The heat transfer enhances enormously when nano-particles are suspended in liquids like water, ethylene glycol etc. This has substantiated by Das *et al.*, (2006) in their review paper. In this scenario cooling systems demand the very low heat transfer rate through nano – fluids and heat energy systems like automobiles demanding the high heat transfer rate through nano – fluids.

Kuznetsov and Nield (2010) studied the classical problem of free convection boundary layer flow of a viscous and incompressible fluid (Newtonian fluid) past a vertical flat plate to the case of nano-fluids. In these papers the authors have used the nano-fluid model proposed by Buongiorno (2006). Although this author discovered that seven slip mechanisms take place in the convective transport in nano-fluids, it is only the Brownian diffusion and the thermophoresis that are the most important when the turbulent flow effects are absent. More recently, Khan and Aziz (2011) studied Natural convection flow of a nano-fluid over a vertical plate with uniform surface heat flux. Hamad and Pop (2011) presented in their recent paper that the solid volume and heat source enhances the heat transfer rate. This brief survey clearly indicates that a definitive conclusion regarding the role of nano-particles in enhancing natural convective transport is yet to be reached.

In this paper we aim to investigate the MHD Cu – water nano-fluid flow and the heat transfer past a vertical infinite permeable inclined oscillating flat plate under heat source, suction and radiation.

## **MATHEMATICAL FORMULATION**

Consider the unsteady three dimensional free convection flow of a nano-fluid past a vertical permeable semi-infinite plate in the presence of an applied magnetic field with constant heat source and radiation. We consider a Cartesian coordinate system  $(\bar{x}, \bar{y}, \bar{z})$ . The flow is assumed to be in the  $\bar{x}$  direction, which is taken along the plate, and  $\bar{z}$  - axis is normal to the plate. We assume that the plate has an oscillatory movement on time  $\bar{t}$  and frequency  $\bar{n}$  with the velocity  $u(0, \bar{t})$ , which is given  $u(0, \bar{t}) = U_0(1 + \varepsilon \cos(n\bar{t}))$ , where  $\varepsilon$  is a small constant parameter ( $\varepsilon \ll 1$ ) and  $U_0$  is the characteristic velocity. We consider that initially ( $\bar{t} < 0$ ) the fluid as well as the plate are at rest. A uniform external magnetic field  $B_0$  is taken to be acting along the  $\bar{z}$  -axis. We consider the case of a short circuit problem in which the applied electric field  $E = 0$ , and also assume that the induced magnetic field is small compared to the external magnetic field  $B_0$ . The surface temperature is assumed to have the constant value  $T_w$  while the ambient temperature has the constant value  $T_\infty$ , where  $T_w > T_\infty$ . The conservation equation of current density  $\nabla \cdot J = 0$  gives  $J_z = \text{constant}$ . Since the plate is electrically non-conducting, this constant is zero. It is assumed that the plate is infinite in extent and hence all physical quantities do not depend on  $\bar{x}$  and  $\bar{y}$  but depend only on  $\bar{z}$  and  $\bar{t}$ ,

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$$\text{i.e } \frac{\partial u}{\partial x} = \frac{\partial u}{\partial y} = 0$$

It is further assumed that the regular fluid and the suspended nano-particles are in thermal equilibrium and no slip occurs between them. Under Bossinesq and boundary layer approximations, the boundary layer equations governing the flow and temperature are,

$$\frac{\partial w}{\partial z} = 0 \quad \dots\dots\dots (1)$$

$$\frac{\partial u}{\partial t} + w \frac{\partial u}{\partial z} = \frac{1}{\rho_{nf}} \left[ \mu_{nf} \frac{\partial^2 u}{\partial z^2} + (\rho \beta)_{nf} g (T - T_\infty) \cos \gamma - \sigma B_0^2 u \right] \quad \dots\dots\dots (2)$$

$$\frac{\partial T}{\partial t} + w \frac{\partial T}{\partial z} = \alpha_{nf} \frac{\partial^2 T}{\partial z^2} - \frac{Q}{(\rho c_p)_{nf}} (T - T_\infty) - \frac{\alpha_{nf}}{(\rho c_p)_{nf}} \frac{\partial q_r}{\partial z} \quad \dots\dots\dots (3)$$

The appropriate initial and boundary conditions for the problem are given by

$$\left. \begin{aligned} u(z, t) = 0, T = T_\infty \text{ for } t < 0 \quad \forall z \\ u(0, t) = \left[ 1 + \frac{\varepsilon}{2} (e^{int} + e^{-int}) \right], T(0, t) = T_w \\ u(\infty, t) \rightarrow 0, T(\infty, t) \rightarrow T_\infty, \quad \varepsilon \ll 1 \end{aligned} \right\} t \geq 0 \quad \dots\dots\dots (4)$$

Thermo-Physical properties are related as follows:

$$\rho_{nf} = (1 - \phi) \rho_f + \phi \rho_s, \quad \mu_{nf} = \frac{\mu_f}{(1 - \phi)^{2.5}}, \quad \alpha_{nf} = \frac{k_{nf}}{(\rho c_p)_{nf}}$$

$$(\rho c_p)_{nf} = (1 - \phi) (\rho c_p)_f + \phi (\rho c_p)_s,$$

$$(\rho \beta)_{nf} = (1 - \phi) (\rho \beta)_f + \phi (\rho \beta)_s,$$

$$k_{nf} = k_f \left[ \frac{k_s + 2k_f - 2\phi(k_f - k_s)}{k_s + 2k_f + 2\phi(k_f - k_s)} \right] \quad \dots\dots\dots (5)$$

The thermo-physical properties of the materials used are as follows.

**Table 1: Thermo-physical properties**

Physical Properties	Water	Copper(Cu)
$C_p$ (J/kg K)	4,179	385
$\rho$ ( $kg/m^3$ )	997.1	8,933
$\kappa$ (W/m K)	0.613	400
$\beta \times 10^{-5}$ (1/K)	21	1.67

We consider the solution of Esq. (1) as  $w = -w_0 \quad \dots\dots\dots (6)$

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where the constant  $w_0$  represents the normal velocity at the plate which is positive for suction ( $w_0 > 0$ ) and negative for blowing or injection ( $w_0 < 0$ ). Thus, we introduce the following dimensionless variables:

$$z = \left(\frac{\psi_f}{U_0}\right)Z, \quad t = \left(\frac{\psi_f}{U_0^2}\right)t^*, \quad n = \left(\frac{U_0^2}{\psi_f}\right)\eta, \quad u = UU_0, \quad \theta = \frac{T - T_\infty}{T_w - T_\infty},$$

$$q_r = -\frac{4\sigma_1}{3\delta} \frac{\partial T^4}{\partial y} \dots\dots\dots (7)$$

We assume that the temperature differences within the flow are sufficiently small so that the  $T^4$  can be expressed as a linear function after using Taylor series to expand  $T^4$  about the free stream temperature  $T_\infty$  and neglecting higher-order terms. This result is the following approximation:

$$T^4 \cong 4T_\infty^3 - 3T_\infty^4$$

By using above, we obtain

$$\frac{\partial q_r}{\partial z} = -\frac{16\sigma_1}{3\delta} \frac{\partial^2 T^4}{\partial z^2} \dots\dots\dots (8)$$

Using equations 5, 6, 7 and 8 the Eqs. 2-3 can be written in the following dimensionless form:

$$\left[1 - \phi + \phi \left(\frac{\rho_s}{\rho_f}\right)\right] \left(\frac{\partial U}{\partial \tau} - S \frac{\partial U}{\partial Z}\right) = \frac{1}{(1-\phi)^{2.5}} \frac{\partial^2 U}{\partial Z^2} + \left[1 - \phi + \phi \frac{(\rho\beta)_s}{(\rho\beta)_f}\right] \theta \cos \gamma - MU \dots\dots\dots (9)$$

$$\left[1 - \phi + \phi \frac{(\rho c_p)_s}{(\rho c_p)_f}\right] \left(\frac{\partial \theta}{\partial \tau} - S \frac{\partial \theta}{\partial Z}\right) = \frac{1}{p_r} \left[\frac{k_{nf}}{k_f} \frac{\partial^2 \theta}{\partial Z^2}\right] - \frac{1}{p_r} Q_H \theta + \frac{1}{p_r} \frac{4}{3} R_a \frac{\partial^2 \theta}{\partial Z^2} \dots\dots\dots (10)$$

where the corresponding boundary conditions (4) can be written in the dimensionless form as:

$$\left. \begin{aligned} U(z,t) = 0, \theta(z,t) = 0 \quad \text{for } t < 0 \forall z \\ U(0,t) = \left[1 + \frac{\varepsilon}{2}(e^{int} + e^{-int})\right], \theta(0,t) = 1 \\ U(\infty,t) \rightarrow 0, \theta(\infty,t) \rightarrow 0 \end{aligned} \right\} \forall t \geq 0 \dots\dots\dots (11)$$

Here  $p_r$  is the Prandtl number,  $S$  is the suction ( $S > 0$ ) or injection ( $S < 0$ ) parameter,  $M$  is the magnetic parameter,  $R_a$  is the Radiation parameter and  $Q_H$  is the heat source parameter, which are defined as:

$$p_r = \frac{\psi_f}{\alpha_f}, \quad S = \frac{w_0}{U_0}, \quad M = \frac{\sigma B_0^2 \psi_f}{\rho_f U_0^2}, \quad R_a = \frac{4\alpha\sigma_1 T_\infty^3}{\delta k_{nf}}, \quad Q_H = \frac{Q \psi_f^2}{k_f U_0^2}$$

where the velocity characteristic  $U_0$  is defined as

$$U_0 = \left[g\beta_f(T_w - T_\infty)\psi_f\right]^{1/3} \dots\dots\dots (12)$$

The local Nusselt number  $Nu$  in dimension less form:

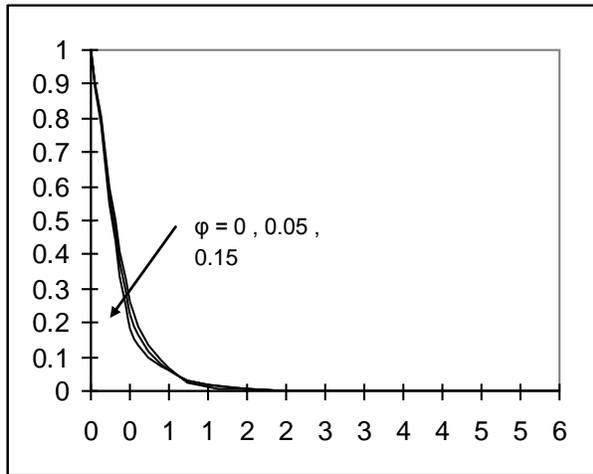
$$Nu = -\frac{k_{nf}}{k_f} \theta'(0) \dots\dots\dots (13)$$

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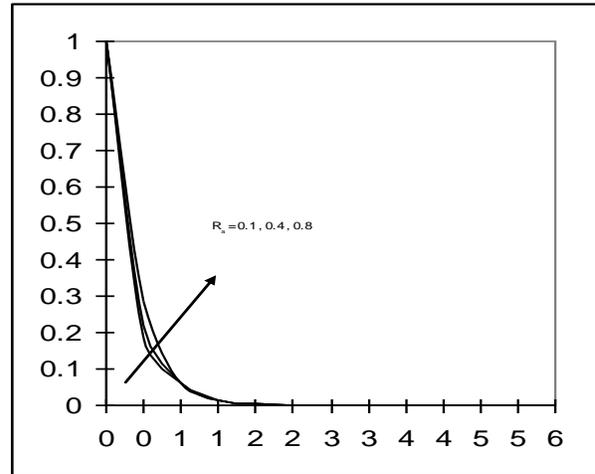
**RESULTS AND DISCUSSIONS**

The governing equations are solved by using Method of lines with the help of Mathematica *package*. The variations of velocity  $U$  and temperature  $\theta$  are graphically exhibited and the Heat Transfer rate ( $Nu$ ) is exhibited in Table – 2 for various values of  $\phi$ ,  $S$ ,  $M$ ,  $\alpha$ ,  $Q_H$  and  $R_a$  by keeping  $Pr = 6.2$ ,  $nt = \pi/2$  and  $\varepsilon = 0.02$ . The effect of various parameters is as follows.

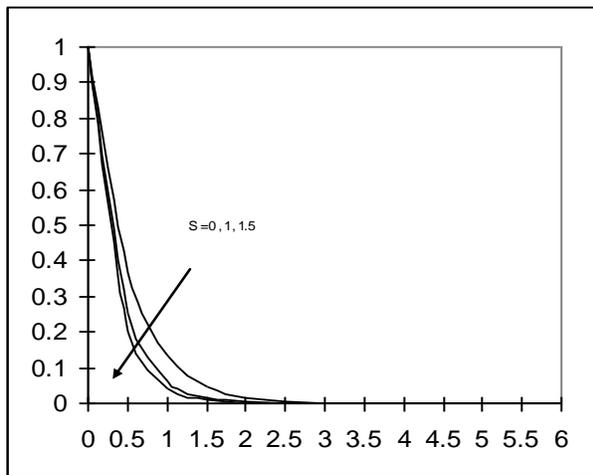
The increase of solid volume fraction reduces the velocity Fig.1 and enhances the temperature Fig.7. The thickness of momentum and the thermal boundary layers decreases with increase in  $\phi$ . The variations of velocity and the temperature with  $R_a$  are depicted in Fig. 2 and 8. The increase in  $R_a$  enhances the momentum and thermal boundary layers.



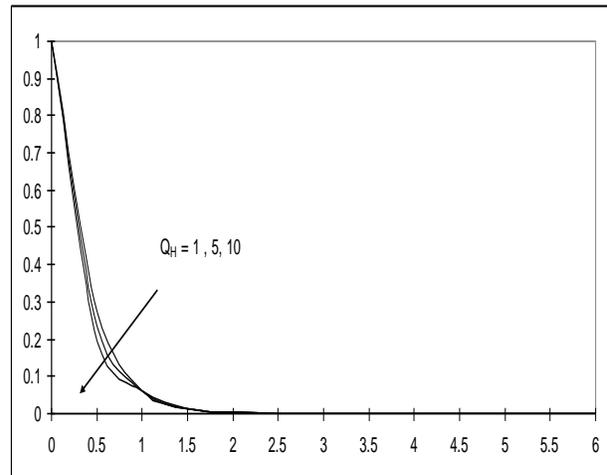
**Figure 1: Variation of U with  $\phi$**



**Figure 2: Variation of U with  $R_a$**



**Figure 3: Variation of U with  $S$**

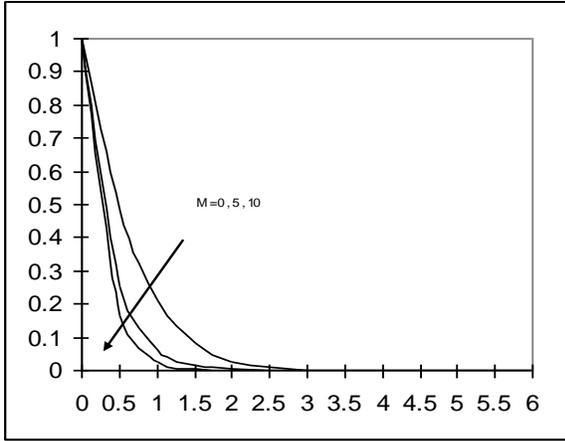


**Figure 4: Variation of U with  $Q_H$**

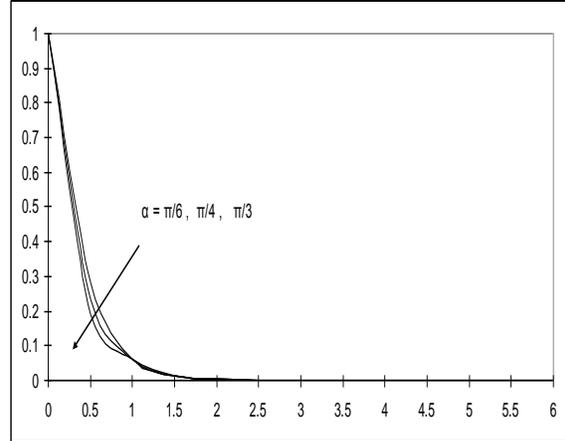
The increase in suction reduces the momentum and thermal boundary layer in Fig. 3 and 9. The variations of velocity and temperature with heat source  $Q_H$  are exhibited in Fig. 4 and 10. The increase in  $Q_H$  decreases the velocity and the temperature. The variations of velocity and temperature with magnetic parameter  $M$  are depicted in Fig. 5 and 11. The effects of inclination angle  $\alpha$  on velocity and temperature are exhibited in Fig. 6 and 12. The increase in inclination reduces the velocity and enhances the temperature.

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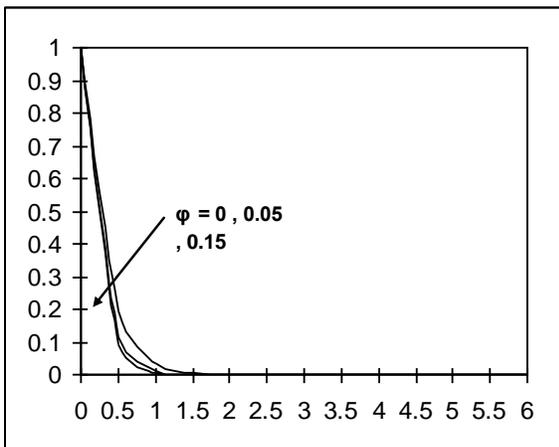
The rate of heat transfer (Nu) for various values of  $R_a$ ,  $\phi$  and  $Q_H$  are given in the Table-2. The Nu is increasing with increase in  $\phi$  and  $Q_H$ . But Nu decreases with increase in  $R_a$ .



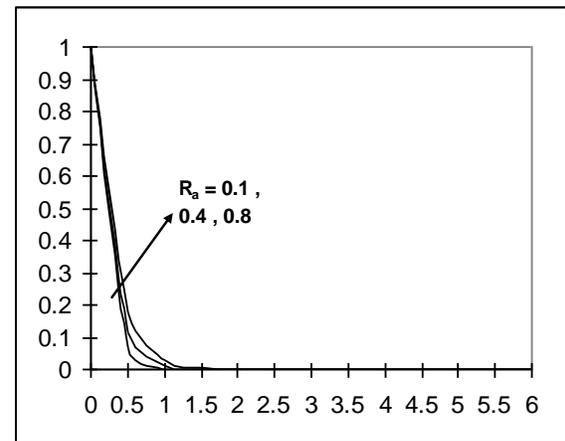
**Figure 5: Variation of U with M**



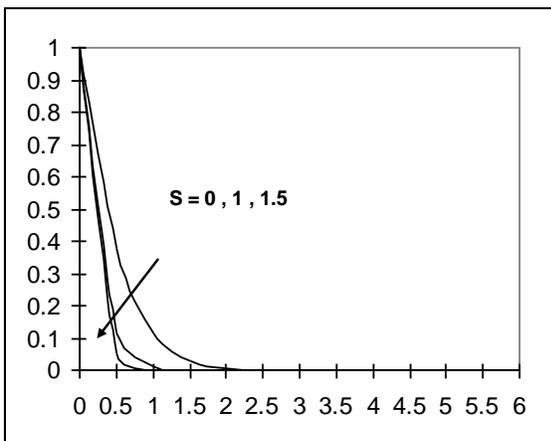
**Figure 6: Variation of U with  $\alpha$**



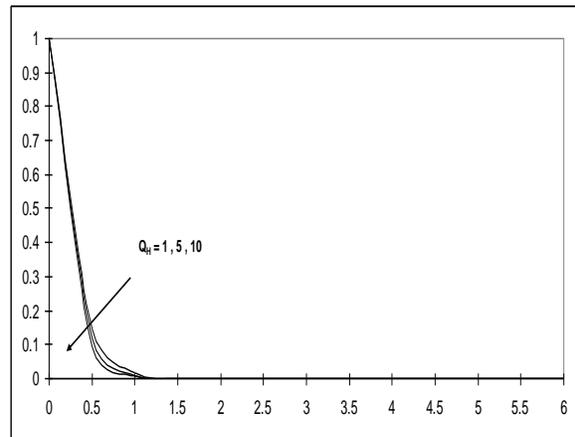
**Figure 7: Variation of  $\theta$  with  $\phi$**



**Figure 8: Variation of  $\theta$  with  $R_a$**

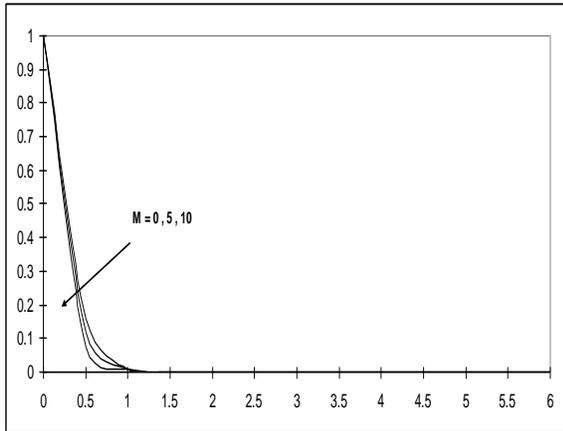


**Figure 9: Variation of  $\theta$  with S**

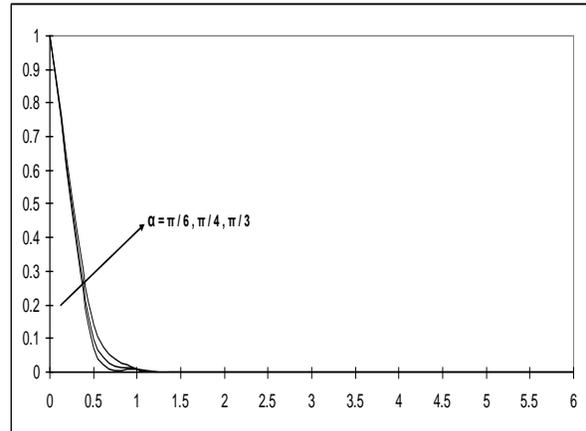


**Figure 10: Variation of  $\theta$  with  $Q_H$**

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**Figure 11: Variation of  $\theta$  with  $M$**



**Figure 12: Variation of  $\theta$  with  $\alpha$**

**Table 2: Nusselt Number**

$\phi$	$Q_H = 5; Ra = 0.4$	$Q_H = 10; Ra = 0.4$	$Q_H = 5; Ra = 0.8$
0	4. 5034	4. 8933	3. 6028
0.05	4. 9525	5. 4462	4. 0485
0.15	5. 8815	6. 6397	5. 0378
0.2	6. 3913	7. 3178	5. 6092

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